

6 Introduction to formal statistical inference

Formal statistical inference uses probability theory to quantify the reliability of data-based conclusions. We want information on a population. We can use:

↓
for example: true mean fill weight of food jars.
average number of cycles to failure of a kind of spring
true mean breaking strength of a wire rope

1. Point estimates:

e.g. sample mean

For example, measure breaking strength of 6 wire ropes as
5, 3, 7, 3, 10, 1

$$\text{estimate } \mu \approx \bar{x} = \frac{5+3+7+3+10+1}{6} = 4.83 \text{ tons.}$$

2. Interval estimates:

μ is likely to be inside the interval $(4.83-2, 4.83+2) = (2.83, 6.83)$

We are confident that the true mean breaking strength μ is somewhere in $(2.83, 6.83)$.

But, how confident?

6.1 Large-sample confidence intervals for a mean

Many important engineering applications of statistics fit the following mold. Values for parameters of a data-generating process are unknown. Based on data, the goal is

1. identify an interval of values likely to contain an unknown parameter
2. quantify "how likely" the interval is to cover the correct value.

Definition 6.1. A *confidence interval* for a parameter (or function of one or more parameters) is a data-based interval of numbers thought likely to contain the parameter (or function of one or more parameters) possessing a stated probability-based confidence or reliability.

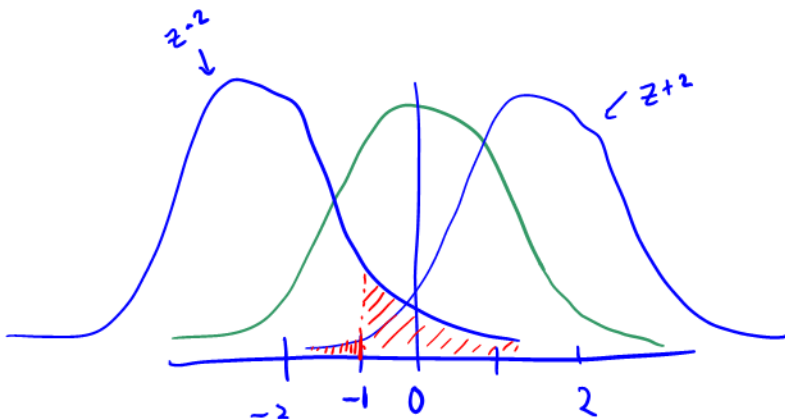
A confidence interval is a realization of a **random interval**, an interval on the real line with a random variable at one or both of the endpoints.

Example 6.1 (Instrumental drift). Let Z be a measure of instrumental drift of a random voltmeter that comes out of a certain factory. Say $Z \sim N(0, 1)$. Define a random interval:

$$\underline{(Z - 2, Z + 2)}$$

What is the probability that -1 is inside the interval?

$$\begin{aligned}
 P(-1 \text{ in } (Z-2, Z+2)) &= P(Z-2 < -1 < Z+2) \\
 &= P(Z-1 < 0 < Z+3) \\
 &= P(-1 < -Z < 3) \quad \text{multiply by } -1 \\
 &= P(-3 < Z < 1) \\
 &= P(Z \leq 1) - P(Z \leq -3) \\
 &= \Phi(1) - \Phi(-3) \\
 &= 0.84
 \end{aligned}$$



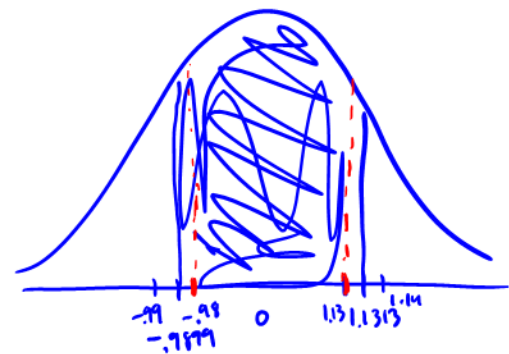
Example 6.2 (More practice). Calculate:

1. $P(2 \text{ in } (X-1, X+1)), X \sim N(2, 4) = 2^2$

$$\begin{aligned}
 P(2 \in (X-1, X+1)) &= P(X-1 < 2 < X+1) \\
 &= P(-1 < 2-X < 1) \quad \left. \begin{array}{l} \text{subtract } X \\ \text{multiply by } -1 \end{array} \right\} \\
 &= P(-1 < X-2 < 1) \\
 &= P\left(-\frac{1}{2} < \frac{X-2}{2} < \frac{1}{2}\right) \quad \left. \begin{array}{l} \text{divide by } \sigma \\ \text{recognize standardized} \end{array} \right\} \\
 &= P(-0.5 < Z < 0.5) \quad Z \sim N(0,1) \\
 &= \Phi(0.5) - \Phi(-0.5) \\
 &= 0.6915 - 0.3085 \\
 &= 0.383
 \end{aligned}$$

2. $P(6.6 \text{ in } (X-2, X+1)), X \sim N(7, 2)$

$$\begin{aligned}
 P(6.6 \in (X-2, X+1)) &= P(X-2 < 6.6 < X+1) \\
 &= P(-2 < 6.6-X < 1) \\
 &= P(-1 < X-6.6 < 2) \\
 &= P(-1.4 < X-7 < 1.6) \\
 &= P\left(-\frac{1.4}{\sqrt{2}} < \frac{X-7}{\sqrt{2}} < \frac{1.6}{\sqrt{2}}\right) \\
 &= P(-0.9899 < Z < 1.1313) \quad Z \sim N(0,1) \\
 &\approx P(-.98 < Z < 1.13) \\
 &= \Phi(1.13) - \Phi(-.98) \\
 &= 0.8708 - 0.1635 = 0.7073
 \end{aligned}$$



"at least"

Example 6.3 (Abstract random intervals). Let's say X_1, X_2, \dots, X_n are iid with $n \geq 25$, mean μ , variance σ^2 . We can find a random interval that provides a lower bound for μ with $1 - \alpha$ probability:

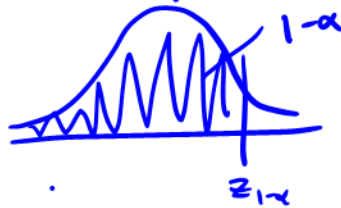
Want a s.t. $P(\mu \in (a, \infty)) = 1 - \alpha$

We know $\bar{X} \sim N(\mu, \frac{\sigma^2}{\sqrt{n}})$ by CLT

$\Rightarrow \left(\frac{\bar{X} - \mu}{\sigma^2/\sqrt{n}} \right) \sim N(0,1)$ by standardization

Let $z_{1-\alpha}$ denote the $1-\alpha$ quantile of $N(0,1)$

$z \sim N(0,1), P(Z \leq z_{1-\alpha}) = 1 - \alpha$



$\Rightarrow P\left(\frac{\bar{X} - \mu}{\sigma^2/\sqrt{n}} \leq z_{1-\alpha}\right) \approx 1 - \alpha$

$P\left(\bar{X} - \mu \leq z_{1-\alpha} \frac{\sigma^2}{\sqrt{n}}\right) \approx 1 - \alpha$

$P\left(\bar{X} - z_{1-\alpha} \frac{\sigma^2}{\sqrt{n}} \leq \mu\right) \approx 1 - \alpha$

$P\left(\mu \in \left(\bar{X} - z_{1-\alpha} \frac{\sigma^2}{\sqrt{n}}, \infty\right)\right) \approx 1 - \alpha$

random variable

Calculate:

$$1. P(\mu \in (-\infty, \bar{X} + z_{1-\alpha} \frac{\sigma}{\sqrt{n}})), X \sim N(\mu, \sigma^2)$$

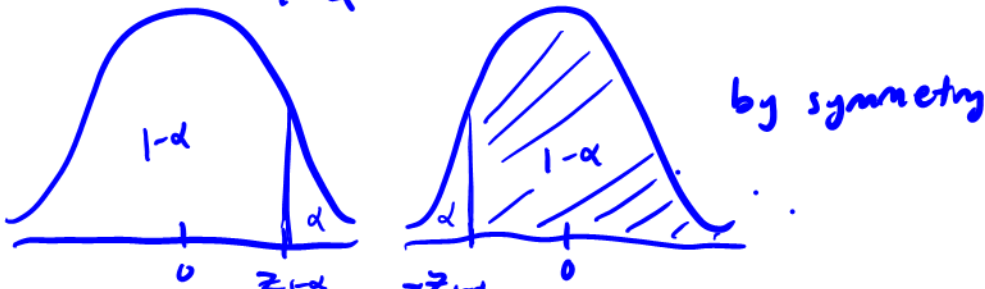
$$= P(\mu < \bar{X} + z_{1-\alpha} \frac{\sigma}{\sqrt{n}})$$

$$= P(-z_{1-\alpha} \frac{\sigma}{\sqrt{n}} < \bar{X} - \mu)$$

$$= P(-z_{1-\alpha} < \frac{\bar{X} - \mu}{\sigma/\sqrt{n}})$$

$$\approx P(-z_{1-\alpha} < Z) \quad Z \sim N(0,1) \text{ by CLT if } n \geq 25$$

$$= 1 - \alpha$$



$$2. P(\mu \in (\bar{X} - z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}}, \bar{X} + z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}})), X \sim N(\mu, \sigma^2)$$

$$= P(\bar{X} - z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}} < \mu < \bar{X} + z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}})$$

$$= P(-z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}} < \mu - \bar{X} < z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}})$$

$$= P(-z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}} < \bar{X} - \mu < z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}})$$

$$= P(-z_{1-\alpha/2} < \frac{\bar{X} - \mu}{\sigma/\sqrt{n}} < z_{1-\alpha/2})$$

standardization
 $\frac{X - E X}{\sqrt{\text{Var} X}}$, mean 0
 variance 1

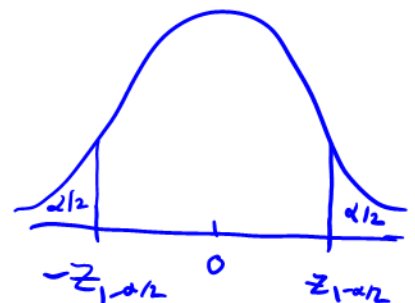
$$\approx P(-z_{1-\alpha/2} < Z < z_{1-\alpha/2}) \quad Z \sim N(0,1) \text{ by CLT for } n \geq 25$$

$Z \sim N(0,1)$ by CLT for $n \geq 25$

$$= \Phi(z_{1-\alpha/2}) - \Phi(-z_{1-\alpha/2})$$

$$= 1 - \frac{\alpha}{2} - \frac{\alpha}{2}$$

$$= 1 - \alpha$$



6.1.1 A Large- n confidence interval for μ involving σ

A $1 - \alpha$ **confidence interval** for an unknown parameter is the realization of a random interval that contains that parameter with probability $1 - \alpha$.

called "confidence level"

For random variables X_1, X_2, \dots, X_n iid with $E(X_1) = \mu$, $\text{Var}(X_1) = \sigma^2$, a $1 - \alpha$ confidence interval for μ is

$n \geq 25$

$$\left(\bar{x} - z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}}, \bar{x} + z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}} \right)$$

depends on data

which is a **realization** from the random interval *(has random variables as endpoints)*

$$\left(\bar{X} - z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}}, \bar{X} + z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}} \right).$$

- Two-sided $1 - \alpha$ confidence interval for μ

$$\left(\bar{x} - z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}}, \bar{x} + z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}} \right)$$

$$\bar{x} \pm z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}}$$

- One-sided $1 - \alpha$ confidence interval for μ with a upper confidence bound

$$\left(-\infty, \bar{x} + z_{1-\alpha} \frac{\sigma}{\sqrt{n}} \right)$$

- One-sided $1 - \alpha$ confidence interval for μ with a lower confidence bound

$$\left(\bar{x} - z_{1-\alpha} \frac{\sigma}{\sqrt{n}}, \infty \right)$$

Example 6.4 (Fill weight of jars). Suppose a manufacturer fills jars of food using a stable filling process with a known standard deviation of $\sigma = 1.6\text{g}$. We take a sample of $n = 47$ jars and measure the sample mean weight $\bar{x} = 138.2\text{g}$. A two-sided 90% confidence interval ($\alpha = 0.1$) for the true mean weight μ is:

$$\begin{aligned} & \left(\bar{x} - z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}}, \bar{x} + z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}} \right) \\ & = \left(138.2 - z_{.95} \frac{1.6}{\sqrt{47}}, 138.2 + z_{.95} \frac{1.6}{\sqrt{47}} \right) \\ & = (138.2 - 1.64(0.23), 138.2 + 1.64(0.23)) \\ & = (137.82, 138.58) \end{aligned}$$

could also write as $138.2 \pm 0.38\text{g}$

Interpretation:

→ We are 90% confident that the true mean fill is between 137.82 and 138.58g.

If we took 100 more samples of 47 jars each, roughly 90 of those samples would produce confidence intervals containing the true mean fill weight.

What if we just want to be sure that the true mean fill weight is high enough?

We could use a one-sided 90% CI with a lower bound.

$$\begin{aligned} & (\bar{x} - z_{1-\alpha} \frac{s}{\sqrt{n}}, \infty) \\ & = (138.2 - z_{.9} \frac{1.6}{\sqrt{47}}, \infty) \\ & = (138.2 - 1.28(0.23), \infty) \\ & = (137.91, \infty) \end{aligned}$$

We are 90% confident that the true mean fill weight is above 137.91.

Example 6.5 (Hard disk failures). F. Willett, in the article "The Case of the Derailed Disk Drives?" (*Mechanical Engineering*, 1988), discusses a study done to isolate the cause of link code A failure in a model of Winchester hard disk drive. For each disk, the investigator measured the breakaway torque (in. oz.) required to loosen the drive's interrupter flag on the stepper motor shaft. Breakaway torques for 26 disk drives were recorded, with a sample mean of 11.5 in. oz. Suppose you know the true standard deviation of the breakaway torques is 5.1 in. oz. Calculate and interpret:

1. A two-sided 90% confidence interval for the true mean breakaway torque of the relevant type of Winchester drive.

$$\begin{aligned} \sigma &= 5.1, \bar{x} = 11.5, n = 26, 1 - \alpha = 0.9 \Rightarrow \alpha = 0.1 \\ &= \left(\bar{x} - Z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}}, \bar{x} + Z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}} \right) \text{ "margin of error"} \\ &= \left(11.5 - Z_{0.95} \frac{5.1}{\sqrt{26}}, 11.5 + Z_{0.95} \frac{5.1}{\sqrt{26}} \right) \\ &= (11.5 - 1.65(1.0002), 11.5 + 1.65(1.0002)) \\ &= (9.85, 13.15) \end{aligned}$$

We are 90% confident that μ (true mean breakaway torque of Winchester drives) is between 9.85 and 13.15 in. oz.

2. An analogous two-sided 95% confidence interval.

$$\begin{aligned} 1 - \alpha &= 0.95 \Rightarrow \alpha = 0.05 \\ &= \left(\bar{x} - Z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}}, \bar{x} + Z_{1-\alpha/2} \frac{\sigma}{\sqrt{n}} \right) \\ &= \left(11.5 - Z_{0.975} \frac{5.1}{\sqrt{26}}, 11.5 + Z_{0.975} \frac{5.1}{\sqrt{26}} \right) \\ &= (9.54, 13.46) \end{aligned}$$

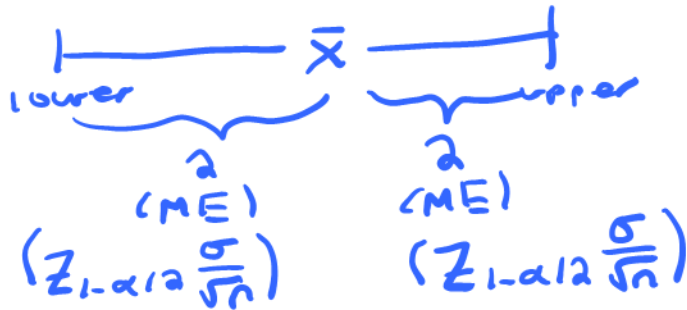
We are 95% confident that μ (true mean breakaway torque of Winchester drives) is between 9.54 and 13.46 in. oz.

With n constant, $\uparrow CL \rightarrow$ wider CI
With CL constant, $\downarrow n \rightarrow$ wider CI

CL = 95%, small M.E (± 2)

Example 6.6 (Width of a CI). If you want to estimate the breakaway torque with a 2-sided, 95% confidence interval with ± 2.0 in. oz. of precision, what sample size would you need?

Interval half-width \rightarrow (M.E)



$$\text{i.e. } Z_{0.975} \frac{5.1}{\sqrt{n}} \leq 2$$

$$1.96 \frac{5.1}{\sqrt{n}} \leq 2$$

$$\frac{9.996}{\sqrt{n}} \leq 2$$

$$n \geq 24.98$$

$$\Rightarrow n \geq 25$$

We should need a sample of at least 25 disks to have at ^{most} a precision of 2 in oz.

6.1.2 A generally applicable large- n confidence interval for μ

Although the equations for a $1 - \alpha$ confidence interval is mathematically correct, it is severely limited in its usefulness because

it requires us to know σ . It is unusual to have to estimate μ (w/ a C.I.), but know σ in real life.

If $n \geq 25$ and σ is *unknown*, $Z = \frac{\bar{X} - \mu}{\sigma/\sqrt{n}}$, where

instead of σ

$$s = \sqrt{\frac{1}{n-1} \sum_{i=1}^n (x_i - \bar{x})^2}.$$

is still **approximately standard normally distributed**. So, you can replace σ in the confidence interval formula with the sample standard deviation, s .

- Two-sided $1 - \alpha$ confidence interval for μ

$$\left(\bar{X} - Z_{1-\alpha/2} \frac{s}{\sqrt{n}}, \bar{X} + Z_{1-\alpha/2} \frac{s}{\sqrt{n}} \right)$$

- One-sided $1 - \alpha$ confidence interval for μ with a upper confidence bound

$$\left(-\infty, \bar{X} + Z_{1-\alpha} \frac{s}{\sqrt{n}} \right)$$

- One-sided $1 - \alpha$ confidence interval for μ with a lower confidence bound

$$\left(\bar{X} - Z_{1-\alpha} \frac{s}{\sqrt{n}}, \infty \right)$$

Example 6.7. Suppose you are a manufacturer of construction equipment. You make 0.0125 inch wire rope and need to determine how much weight it can hold before breaking so that you can label it clearly. Here are breaking strengths, in kg, for 41 sample wires:

[1] 100.37 96.31 72.57 88.02 105.89 107.80 75.84 92.73 67.47 94.87
 [11] 122.04 115.12 95.24 119.75 114.83 101.79 80.90 96.10 118.51 109.66
 [21] 88.07 56.29 86.50 57.62 74.70 92.53 86.25 82.56 97.96 94.92
 [31] 62.00 93.00 98.44 119.37 103.70 72.40 71.29 107.24 64.82 93.51
 [41] 86.97

The sample mean breaking strength is 91.85 kg and the sample standard deviation is 17.6 kg. Using the appropriate 95% confidence interval, try to determine whether the breaking strengths meet the requirement of at least 85 kg.

$$1 - \alpha = 0.95 \Rightarrow \alpha = 0.05$$

$$\bar{X} = 91.85$$

$$s = 17.6$$

$$n = 41$$

$$\left(\bar{X} - Z_{1-\alpha} \frac{s}{\sqrt{n}}, \infty \right)$$

$$= \left(91.85 - Z_{0.95} \frac{17.6}{\sqrt{41}}, \infty \right)$$

$$= \left(91.85 - 1.65 \frac{17.6}{\sqrt{41}}, \infty \right)$$

$$= (87.314, \infty)$$

With 95% confidence, we have shown that μ (the true breaking strength of the wire ropes) is above 87.314 kg.

\Rightarrow hence, the 85 kg requirement is met w/ 95% confidence.

6.2 Small-sample confidence intervals for a mean

The most important practical limitation on the use of the methods of the previous sections is

the requirement that n must be large ($n \geq 25$)

That restriction comes from the fact that without it,

there is no way to conclude $\frac{\bar{x} - \mu}{s/\sqrt{n}} \sim N(0, 1)$

So, if one mechanically uses the large- n interval formula $\bar{x} \pm z \frac{s}{\sqrt{n}}$ with a small sample,

there is no way of assessing what actual level of confidence $(1 - \alpha)$ should be declared.

If it is sensible to model the observations as iid normal random variables, then we can arrive at inference methods for small- n sample means.

if this is true, $\frac{\bar{x} - \mu}{s/\sqrt{n}}$ isn't standard normal,

BUT it is a named distribution.

6.2.1 The Student t distribution

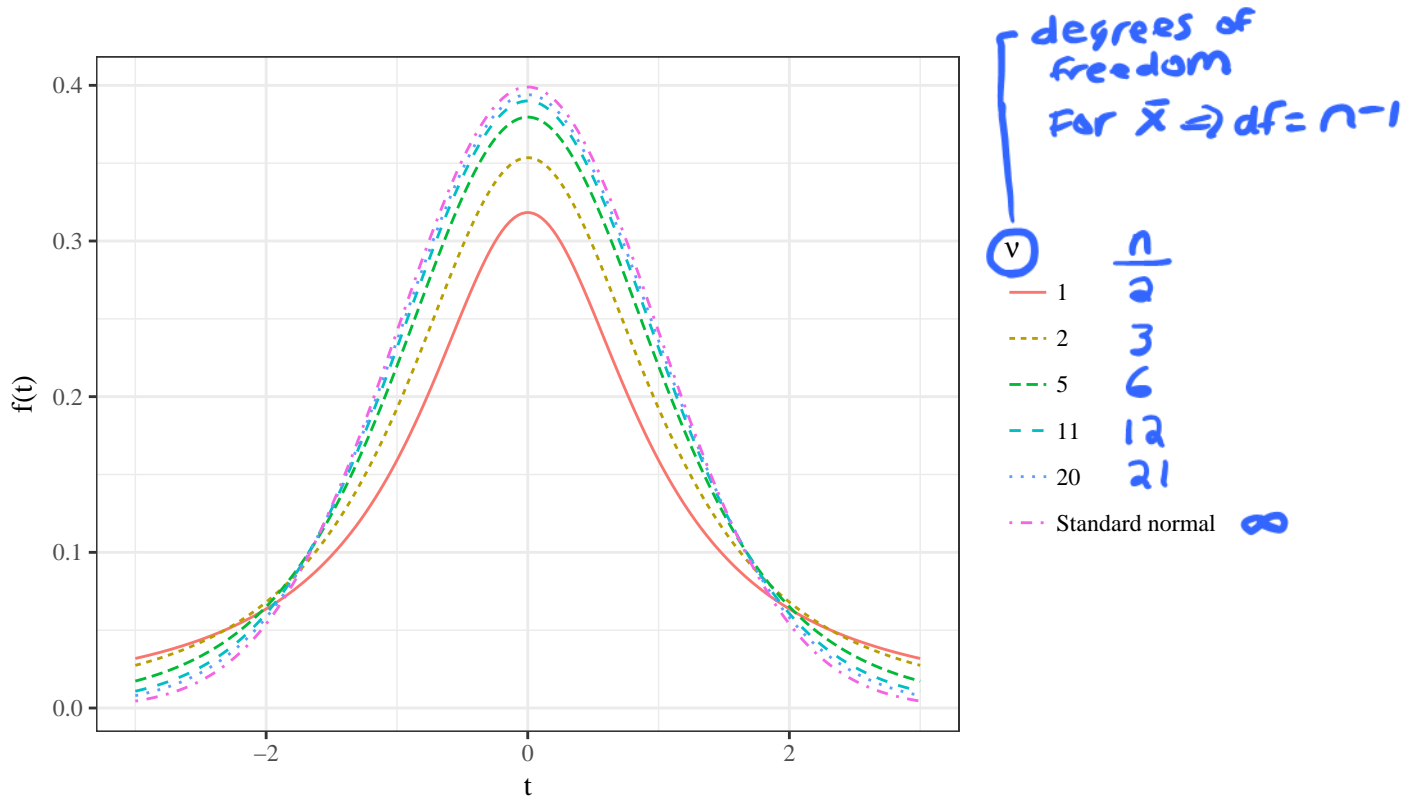
Definition 6.2. The *(Student) t distribution with degrees of freedom parameter ν* is a continuous probability distribution with probability density

$$f(t) = \frac{\Gamma\left(\frac{\nu+1}{2}\right)}{\Gamma\left(\frac{\nu}{2}\right)\sqrt{\pi\nu}} \left(1 + \frac{t^2}{\nu}\right)^{-(\nu+1)/2} \quad \text{for all } t.$$

The t distribution

- is bell-shaped and symmetric about 0
- has fatter tails than the normal, but approaches the shape of the normal as $\nu \rightarrow \infty$.

We use the t table (Table B.4 in Vardeman and Jobe) to calculate quantiles.



t-distn w/ df=5 (n=6)

Example 6.8 (t quantiles). Say $T \sim t_5$. Find c such that $P(T \leq c) = 0.9$.

Table B.4

t Distribution Quantiles

| ν | $Q(.9)$ | $Q(.95)$ | $Q(.975)$ | $Q(.99)$ | $Q(.995)$ | $Q(.999)$ | $Q(.9995)$ |
|-------|---------|----------|-----------|----------|-----------|-----------|------------|
| 1 | 3.078 | 6.314 | 12.706 | 31.821 | 63.657 | 318.317 | 636.607 |
| 2 | 1.886 | 2.920 | 4.303 | 6.965 | 9.925 | 22.327 | 31.598 |
| 3 | 1.638 | 2.353 | 3.182 | 4.541 | 5.841 | 10.215 | 12.924 |
| 4 | 1.533 | 2.132 | 2.776 | 3.747 | 4.604 | 7.173 | 8.610 |
| 5 | 1.476 | 2.015 | 2.571 | 3.365 | 4.032 | 5.893 | 6.869 |

Figure 1: Student's t distribution quantiles.

$$P(T \leq 1.476) = 0.9$$

$Q(p)$ for a t_ν is often denoted as $t_{\nu,p}$.

$$\text{So, } t_{5,0.9} = 1.476$$

6.2.2 Small-sample confidence intervals, σ unknown

If we can assume that X_1, \dots, X_n are iid with mean μ and variance σ^2 , and are also normally distributed,

we can't use CLT since $n < 25$.

But we know $\frac{\bar{X} - \mu}{S/\sqrt{n}} \sim t_{n-1}$ (since X_1, \dots, X_n iid $N(\mu, \sigma^2)$)

side note: If we do know σ , then $\frac{\bar{X} - \mu}{\sigma/\sqrt{n}} \sim N(0, 1)$
even for small n (if X_1, \dots, X_n iid $N(\mu, \sigma^2)$)

We can then use $t_{n-1, \overset{df}{1-\alpha/2}}$ instead of $z_{1-\alpha/2}$ in the confidence intervals.

- Two-sided $1 - \alpha$ confidence interval for μ

$$\left(\bar{X} - t_{n-1, 1-\alpha/2} \frac{s}{\sqrt{n}}, \bar{X} + t_{n-1, 1-\alpha/2} \frac{s}{\sqrt{n}} \right)$$

- One-sided $1 - \alpha$ confidence interval for μ with an upper confidence bound

$$\left(-\infty, \bar{X} + t_{n-1, 1-\alpha} \frac{s}{\sqrt{n}} \right)$$

- One-sided $1 - \alpha$ confidence interval for μ with a lower confidence bound

$$\left(\bar{X} - t_{n-1, 1-\alpha} \frac{s}{\sqrt{n}}, \infty \right)$$

Example 6.9 (Concrete beams). 10 concrete beams were each measured for flexural strength (MPa). Assuming the flexural strengths are iid normal, calculate and interpret a two-sided 99% CI for the flexural strength of the beams.

[1] 8.2 8.7 7.8 9.7 7.4 7.8 7.7 11.6 11.3 11.8

$$n = 10, \alpha = 0.01$$

$$\bar{x} = \frac{1}{10} (8.2 + \dots + 11.8) = 9.2$$

$$s = \sqrt{\frac{1}{9} [(8.2 - 9.2)^2 + \dots + (11.8 - 9.2)^2]} = 1.76$$

$$\begin{aligned} \text{Two-sided } 99\% \text{ CI: } & \left(\bar{x} - t_{n-1, 1-\alpha/2} \frac{s}{\sqrt{n}}, \bar{x} + t_{n-1, 1-\alpha/2} \frac{s}{\sqrt{n}} \right) \\ & = \left(9.2 - t_{9, 0.995} \frac{1.76}{\sqrt{10}}, 9.2 + t_{9, 0.995} \frac{1.76}{\sqrt{10}} \right) \\ & = (9.2 - 3.250 (0.556), 9.2 + 3.250 (0.556)) \\ & \quad (7.393, 11.007) \end{aligned}$$

We are 99% confident that μ (true mean flexural strength of this kind of concrete beam) is between 7.393 MPa and 11.007 MPa.

Is the true mean flexural strength below the minimum requirement of 11 MPa? Find out with the appropriate 95% CI.

$$\begin{aligned} & = (-\infty, \bar{x} + t_{n-1, 1-\alpha} \frac{s}{\sqrt{n}}) \\ & = (-\infty, 9.2 + t_{9, 0.95} \frac{1.76}{\sqrt{10}}) \\ & = (-\infty, 9.2 + 1.833 \frac{1.76}{\sqrt{10}}) \\ & = (-\infty, 10.21) \end{aligned}$$

What if we accidentally tried to solve this problem using a lower-bound CI instead of an upper-bound CI?

$$(\bar{x} - t_{n-1, 1-\alpha} \frac{s}{\sqrt{n}}, \infty)$$

This would be a problem b/c our answer would be (c, ∞) , where c is a constant lower-bound. A part of interval (c, ∞) will always contain estimates of μ greater than 11 (since $\infty > 11$), and the minimal requirement of 11 will always pass.

We are 95% confident that μ (true mean flexural strength of this kind of concrete beam) is below 10.21 MPa. (That's below 11 MPa)

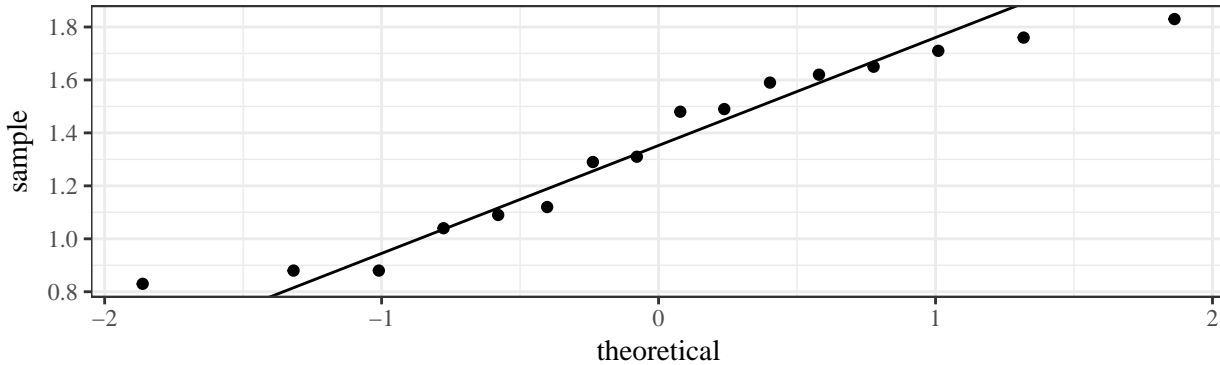
At $\alpha = 0.05$, we have shown the true mean flexural strength is < 11 MPa, and the minimal requirement is not met.

Example 6.10 (Paint thickness). Consider the following sample of observations on coating thickness for low-viscosity paint.

[1] 0.83 0.88 0.88 1.04 1.09 1.12 1.29 1.31 1.48 1.49 1.59 1.62 1.65 1.71

[15] 1.76 1.83

A normal QQ plot shows that they are close enough to normally distributed.



Calculate and interpret a two-sided 90% confidence interval for the true mean thickness.

$$n=16, \alpha=0.1$$

$$\bar{X} = \frac{1}{16} (0.83 + \dots + 1.83) = 1.35 \text{ mm}$$

$$S = \sqrt{\frac{1}{15} [(0.83 - 1.35)^2 + \dots + (1.83 - 1.35)^2]} = 0.34 \text{ mm}$$

$$= \left(\bar{X} - t_{n-1, 1-\alpha/2} \frac{S}{\sqrt{n}}, \bar{X} + t_{n-1, 1-\alpha/2} \frac{S}{\sqrt{n}} \right)$$

$$= \left(1.35 - t_{15, 0.95} \frac{0.34}{\sqrt{16}}, 1.35 + t_{15, 0.95} \frac{0.34}{\sqrt{16}} \right)$$

$$= \left(1.35 - 1.753 \frac{0.34}{\sqrt{16}}, 1.35 + 1.753 \frac{0.34}{\sqrt{16}} \right)$$

$$= (1.201, 1.499)$$

We are 90% confident that μ (true mean thickness) is between 1.201 and 1.499 mm.

Table B.4
t Distribution Quantiles

| ν | $Q(.9)$ | $Q(.95)$ | $Q(.975)$ | $Q(.99)$ | $Q(.995)$ | $Q(.999)$ | $Q(.9995)$ |
|----------|---------|----------|-----------|----------|-----------|-----------|------------|
| 1 | 3.078 | 6.314 | 12.706 | 31.821 | 63.657 | 318.317 | 636.607 |
| 2 | 1.886 | 2.920 | 4.303 | 6.965 | 9.925 | 22.327 | 31.598 |
| 3 | 1.638 | 2.353 | 3.182 | 4.541 | 5.841 | 10.215 | 12.924 |
| 4 | 1.533 | 2.132 | 2.776 | 3.747 | 4.604 | 7.173 | 8.610 |
| 5 | 1.476 | 2.015 | 2.571 | 3.365 | 4.032 | 5.893 | 6.869 |
| 6 | 1.440 | 1.943 | 2.447 | 3.143 | 3.707 | 5.208 | 5.959 |
| 7 | 1.415 | 1.895 | 2.365 | 2.998 | 3.499 | 4.785 | 5.408 |
| 8 | 1.397 | 1.860 | 2.306 | 2.896 | 3.355 | 4.501 | 5.041 |
| 9 | 1.383 | 1.833 | 2.262 | 2.821 | 3.250 | 4.297 | 4.781 |
| 10 | 1.372 | 1.812 | 2.228 | 2.764 | 3.169 | 4.144 | 4.587 |
| 11 | 1.363 | 1.796 | 2.201 | 2.718 | 3.106 | 4.025 | 4.437 |
| 12 | 1.356 | 1.782 | 2.179 | 2.681 | 3.055 | 3.930 | 4.318 |
| 13 | 1.350 | 1.771 | 2.160 | 2.650 | 3.012 | 3.852 | 4.221 |
| 14 | 1.345 | 1.761 | 2.145 | 2.624 | 2.977 | 3.787 | 4.140 |
| 15 | 1.341 | 1.753 | 2.131 | 2.602 | 2.947 | 3.733 | 4.073 |
| 16 | 1.337 | 1.746 | 2.120 | 2.583 | 2.921 | 3.686 | 4.015 |
| 17 | 1.333 | 1.740 | 2.110 | 2.567 | 2.898 | 3.646 | 3.965 |
| 18 | 1.330 | 1.734 | 2.101 | 2.552 | 2.878 | 3.610 | 3.922 |
| 19 | 1.328 | 1.729 | 2.093 | 2.539 | 2.861 | 3.579 | 3.883 |
| 20 | 1.325 | 1.725 | 2.086 | 2.528 | 2.845 | 3.552 | 3.849 |
| 21 | 1.323 | 1.721 | 2.080 | 2.518 | 2.831 | 3.527 | 3.819 |
| 22 | 1.321 | 1.717 | 2.074 | 2.508 | 2.819 | 3.505 | 3.792 |
| 23 | 1.319 | 1.714 | 2.069 | 2.500 | 2.807 | 3.485 | 3.768 |
| 24 | 1.318 | 1.711 | 2.064 | 2.492 | 2.797 | 3.467 | 3.745 |
| 25 | 1.316 | 1.708 | 2.060 | 2.485 | 2.787 | 3.450 | 3.725 |
| 26 | 1.315 | 1.706 | 2.056 | 2.479 | 2.779 | 3.435 | 3.707 |
| 27 | 1.314 | 1.703 | 2.052 | 2.473 | 2.771 | 3.421 | 3.690 |
| 28 | 1.313 | 1.701 | 2.048 | 2.467 | 2.763 | 3.408 | 3.674 |
| 29 | 1.311 | 1.699 | 2.045 | 2.462 | 2.756 | 3.396 | 3.659 |
| 30 | 1.310 | 1.697 | 2.042 | 2.457 | 2.750 | 3.385 | 3.646 |
| 40 | 1.303 | 1.684 | 2.021 | 2.423 | 2.704 | 3.307 | 3.551 |
| 60 | 1.296 | 1.671 | 2.000 | 2.390 | 2.660 | 3.232 | 3.460 |
| 120 | 1.289 | 1.658 | 1.980 | 2.358 | 2.617 | 3.160 | 3.373 |
| ∞ | 1.282 | 1.645 | 1.960 | 2.326 | 2.576 | 3.090 | 3.291 |

This table was generated using MINITAB.